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## EXPANDING A TUBULAR MEMBER

### Cross Reference To Related Applications

The present application claims the benefit of the filing date of U.S. provisional patent application serial no. 60/183,546, attorney docket no. 25791.10, filed on 2/18/2000.

- 5        This application is a continuation-in-part of U.S. Serial No. 09/559,122, attorney docket number 25791.23.02, filed on 4/26/2000, which claimed the benefit of the filing date of U.S. provisional patent application serial number 60/131,106, filed on 4/26/1999, which was a continuation-in-part of U.S. patent application serial number 09/523,460, attorney docket number 25791.11.02, filed on 3/10/ 2000, which claimed the benefit of
- 10      the filing date of U.S. provisional patent application serial no. 60/124,042, filed on 3/11/1999, which was a continuation-in-part of U.S. patent application serial number 09/510,913, attorney docket number 25791.7.02, which claimed the benefit of the filing date of U.S. provisional patent application serial number 60/121,702, filed on 2/25/1999, which was a continuation-in-part of U.S. patent application serial number 09/502,350,
- 15      attorney docket number 25791.8.02, filed on 2/10/2000, which claimed the benefit of the filing date of U.S. provisional patent application serial number 60/119,611, attorney docket number 25791.8, filed on 2/11/1999, which was a continuation-in-part of U.S. patent application serial number 09/454,139, attorney docket number 25791.3.02, filed on 12/3/1999, which claimed the benefit of the filing date of U.S. provisional patent
- 20      application serial number 60/111,293, filed on 12/7/1998.

The present application is related to the following U.S. patents and applications:

- (1) utility patent 6,328,113, having application number 09/440,338, attorney docket number 25791.9.02, filed on 11-16-1999, which claimed the benefit of the filing date of provisional patent application number 60/108,558, attorney docket number 25791.9, filed
- 25      on 11-16-1998; (2) utility patent 6,497,289, having application number 09/454,139, attorney docket number 25791.3.02, filed on 12-3-1999, which claimed the benefit of the filing date of provisional patent application number 60/111,293, attorney docket number 25791.3, filed on 12-7-1998; (3) utility patent application number 09/502,350, attorney docket number 25791.8.02, filed on 2-10-2000, which claimed the benefit of the filing
- 30      date of provisional patent application number 60/119,611, attorney docket number 25791.8, filed on 2-11-1999; (4) provisional patent application number 60/121,702,

attorney docket number 25791.7, filed on 2-25-1999; (5) provisional patent application number 60/121,841, attorney docket number 25791.12, filed on 2-26-1999; (6) provisional patent application number 60/121,907, attorney docket number 25791.16, filed on 2-26-1999; (7) provisional patent application number 60/124,042, attorney docket  
5 number 25791.11, filed on 3-11-1999; (8) provisional patent application number 60/131,106, attorney docket number 25791.23, filed on 4-26-1999; (9) provisional patent application number 60/137,998, attorney docket number 25791.17, filed on 6-7-1999; (10) provisional patent application number 60/143,039, attorney docket number 25791.26, filed on 7-9-1999; (11) provisional patent application number 60/146,203, attorney docket  
10 number 25791.25, filed on 7-29-1999; (12) provisional patent application number 60/154,047, attorney docket number 25791.29, filed on 9-16-1999; (13) provisional patent application number 60/159,082, attorney docket number 25791.34, filed on 10-12-1999; (14) provisional patent application number 60/159,039, attorney docket number 25791.36, filed on 10-12-1999; (15) provisional patent application number 60/159,033, attorney  
15 docket number 25791.37, filed on 10-12-1999; (16) provisional patent application number 60/162,671, attorney docket number 25791.27, filed on 11-01-1999.

#### Background of the Invention

This invention relates generally to wellbore casings, and in particular to wellbore  
20 casings that are formed using expandable tubing.

Conventionally, when a wellbore is created, a number of casings are installed in the borehole to prevent collapse of the borehole wall and to prevent undesired outflow of drilling fluid into the formation or inflow of fluid from the formation into the borehole. The borehole is drilled in intervals whereby a casing which is to be installed in a lower  
25 borehole interval is lowered through a previously installed casing of an upper borehole interval. As a consequence of this procedure the casing of the lower interval is of smaller diameter than the casing of the upper interval. Thus, the casings are in a nested arrangement with casing diameters decreasing in downward direction. Cement annuli are provided between the outer surfaces of the casings and the borehole wall to seal the  
30 casings from the borehole wall. As a consequence of this nested arrangement a relatively large borehole diameter is required at the upper part of the wellbore. Such a large

borehole diameter involves increased costs due to heavy casing handling equipment, large drill bits and increased volumes of drilling fluid and drill cuttings. Moreover, increased drilling rig time is involved due to required cement pumping, cement hardening, required equipment changes due to large variations in hole diameters drilled in the course of the well, and the large volume of cuttings drilled and removed.

Conventionally, at the surface end of the wellbore, a wellhead is formed that typically includes a surface casing, a number of production and/or drilling spools, valving, and a Christmas tree. Typically the wellhead further includes a concentric arrangement of casings including a production casing and one or more intermediate casings. The casings are typically supported using load bearing slips positioned above the ground. The conventional design and construction of wellheads is expensive and complex.

Conventionally, a wellbore casing cannot be formed during the drilling of a wellbore. Typically, the wellbore is drilled and then a wellbore casing is formed in the newly drilled section of the wellbore. This delays the completion of a well.

The present invention is directed to overcoming one or more of the limitations of the existing procedures for forming wellbores and wellheads.

#### Summary

According to an aspect of the present invention, there is provided a method of coupling a tubular member to a pre-existing structure, comprising: positioning the tubular member in an overlapping relationship to the pre-existing structure; placing a mandrel within the tubular member; pressurizing a region within the tubular member above the mandrel; and displacing the mandrel with respect to the tubular member.

Preferably, the method further comprises removing fluids within the tubular member that are displaced by the displacement of the mandrel.

Preferably, the removed fluids pass inside the region and the volume of the region increases.

Preferably, the region is sealed off and sealing off the region includes sealing a stationary member and sealing a non-stationary member.

Preferably, the method further includes conveying a first fluid in a first direction along an axis of the tubular member, and a second fluid in a second direction along the axis, the first direction being different than the second direction.

Preferably, the method further includes conveying a pressurized fluid in a first direction along an axis of the tubular member, and a non-pressurized fluid in a second direction along the axis, the first direction being different than the second direction.

Preferably, the pressurizing is provided at operating pressures ranging from 0 to 620.528 bar (0 to 9,000 psi) and at flow rates ranging from 0 to 11356.24 litres/ minute (0 to 3,000 gallons/minute).

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According to another aspect of the present invention, there is provided an apparatus for radially expanding a tubular member, comprising: a first tubular member; a second tubular member positioned within the first tubular member; a third tubular member movably coupled to and positioned within the second tubular member; a first annular sealing member for sealing an interface between the first and second tubular members; a second annular sealing member for sealing an interface between the second and third tubular members; and a mandrel positioned within the first tubular member and coupled to an end of the third tubular member.

Preferably, the apparatus further includes an annular chamber defined by the first tubular member, the second tubular member, the third tubular member, the first annular sealing member, the second annular sealing member, and the mandrel.

Preferably, the apparatus further includes an annular passage defined by the second tubular member and the third tubular member, a fluid passage contained within the third tubular member and the mandrel and one or more sealing members coupled to an exterior 25 surface of the first tubular member.

Preferably, the apparatus further includes an annular chamber defined by the first tubular member, the second tubular member, the third tubular member, the first annular sealing member, the second annular sealing member, and the mandrel; and an annular passage defined by the second tubular member and the third tubular member.

30 Preferably, the annular chamber and the annular passage are fluidically coupled.

Preferably, one or more slips are coupled to the exterior surface of the first tubular member and the mandrel includes a conical surface.

Preferably, the angle of attack of the conical surface ranges from 0 to 30 degrees and the conical surface has a surface hardness ranging from 58 to 62 Rockwell C.

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According to another aspect of the present invention, there is provided an apparatus, comprising: a first tubular member; and a second tubular member coupled to the first tubular member wherein the second tubular member is positioned in an overlapping relationship to the first tubular member; a mandrel within the second tubular member;

10 a pressurized region within the second tubular member above the mandrel; and a mechanism adapted for displacing the mandrel with respect to the second tubular member.

Preferably, the apparatus further comprises a mechanism for removing fluids within the second tubular member that are displaced by the displacement of the mandrel.

15 Preferably, the removed fluids pass inside the pressurized region and preferably, the volume of the pressurized region increases.

Preferably, the apparatus further comprises a sealing mechanism adapted for sealing off the pressurized region and preferably, sealing off the pressurized region includes sealing a stationary member and sealing a non-stationary member.

20 Preferably, the apparatus further comprises a mechanism for conveying a first fluid in a first direction along an axis of the second tubular member, and a second fluid in a second direction along the axis, the first direction being different than the second direction.

25 Preferably, the apparatus further comprises a mechanism for conveying a pressurized fluid in a first direction along an axis of the second tubular member, and a non-pressurized fluid in a second direction along the axis, the first direction being different than the second direction.

Preferably, the pressurizing is provided at operating pressures ranging from 0 to 620.528 bar (0 to 9,000 psi) and at flow rates ranging from 0 to 11356.24 litres/minute (0 to 3,000 gallons/minute).

According to another aspect of the present invention, there is provided a method of coupling a tubular member to a preexisting structure, comprising preforming the tubular member to include a first portion, a second portion and a third portion; placing a mandrel within the second portion of the tubular member; positioning the tubular member in an

5 overlapping relationship to the preexisting structure; pressurizing a region within the tubular member above the mandrel; and displacing the mandrel with respect to the tubular member; wherein the inside diameter of the second portion of the tubular member is greater than the inside diameters of the first and third portions of the tubular member.

Preferably, the pressurizing is provided at operating pressures ranging from 0 to  
10 620.528 bar (0 to 9,000 psi) and at flow rates ranging from 0 to 11356.24 litres/minute (0 to 3,000 gallons/minute).

Preferably, the tubular member is expanded beginning at an upper portion of the tubular member.

15 According to another aspect of the present invention, there is provided an apparatus for radially expanding a tubular member, comprising a first tubular member; a second tubular member coupled to the first tubular member; a third tubular member coupled to the second tubular member; and a mandrel positioned within the second tubular member and coupled to an end portion of the third tubular member; wherein the 20 inside diameter of the second tubular member is greater than the inside diameters of the first and third tubular members.

Preferably, the mandrel includes a fluid passage having an inlet adapted to receive a fluid stop member.

Preferably, the apparatus further includes one or more slips coupled to the exterior 25 surface of the third tubular member.

Preferably, the mandrel includes a conical surface, the angle of attack of the conical surface ranges from 0 to 30 degrees and the conical surface has a surface hardness ranging from 58 to 62 Rockwell C.

30 According to another aspect of the present invention, there is provided an apparatus, comprising: a preexisting structure; and a tubular member coupled to the preexisting

structure, the tubular member to include a first portion a second portion and a third portion; a mandrel within the second portion of the tubular member; the tubular member in an overlapping relationship to the preexisting structure; a pressurized region within the tubular member above the mandrel; and a mechanism for 5 displacing the mandrel with respect to the tubular member; wherein the inside diameter of the second portion of the tubular member is greater than the inside diameters of the first and third portions of the tubular member.

Preferably, the pressurizing is provided at operating pressures ranging from 0 to 620.528 bar (0 to 9,000 psi) and at flow rates ranging from 0 to 11356.24 litres/minute (0 10 to 3,000 gallons/minute).

#### Brief Description of the Drawings

FIG. 1a is a fragmentary cross-section illustration of an embodiment of an apparatus and method for expanding tubular members.

15 FIG. 1b is another fragmentary cross-sectional illustration of the apparatus of FIG. 1a.

FIG. 1c is another fragmentary cross-sectional illustration of the apparatus of FIG. 1a.

20 FIG. 2a is a fragmentary cross-section illustration of an embodiment of an apparatus and method for expanding tubular members.

FIG. 2b is another fragmentary cross-sectional illustration of the apparatus of FIG. 2a.

25 FIG. 2c is another fragmentary cross-sectional illustration of the apparatus of FIG. 2a.

FIG. 2d is another fragmentary cross-sectional illustration of the apparatus of FIG. 2a.

20 FIG. 2e is another fragmentary cross-sectional illustration of the apparatus of FIG. 2a.

#### Detailed Description of the Illustrative Embodiments

30 Referring now to FIGS. 1a, 1b and 1c, an apparatus 100 for expanding a tubular member will be described. In a preferred embodiment, the apparatus 100 includes a

support member 105, a packer 110, a first fluid conduit 115, an annular fluid passage 120, fluid inlets 125, an annular seal 130, a second fluid conduit 135, a fluid passage 140, a mandrel 145, a mandrel launcher 150, a tubular member 155, slips 160, and seals 165. In a preferred embodiment, the apparatus 100 is used to radially expand the tubular member

5 155. In this manner, the apparatus 100 may be used to form a wellbore casing, line a wellbore casing, form a pipeline, line a pipeline, form a structural support member, or repair a wellbore casing, pipeline or structural support member. In a preferred embodiment, the apparatus 100 is used to clad at least a portion of the tubular member 155 onto a preexisting tubular member.

10 The support member 105 is preferably coupled to the packer 110 and the mandrel launcher 150. The support member 105 preferably is a tubular member fabricated from any number of conventional commercially available materials such as, for example, oilfield country tubular goods, low alloy steel, carbon steel, or stainless steel. The support member 105 is preferably selected to fit through a preexisting section of wellbore casing

15 170. In this manner, the apparatus 100 may be positioned within the wellbore casing 170. In a preferred embodiment, the support member 105 is releasably coupled to the mandrel launcher 150. In this manner, the support member 105 may be decoupled from the mandrel launcher 150 upon the completion of an extrusion operation.

The packer 110 is coupled to the support member 105 and the first fluid conduit

20 115. The packer 110 preferably provides a fluid seal between the outside surface of the first fluid conduit 115 and the inside surface of the support member 105. In this manner, the packer 110 preferably seals off and, in combination with the support member 105, first fluid conduit 115, second fluid conduit 135, and mandrel 145, defines an annular chamber 175. The packer 110 may be any number of conventional commercially available packers

25 modified in accordance with the teachings of the present disclosure. In a preferred embodiment, the packer 110 is an RTTS packer available from Halliburton Energy Services in order to optimally provide high load and pressure containment capacity while also allowing the packer to be set and unset multiple times without having to pull the packer out of the wellbore.

30 The first fluid conduit 115 is coupled to the packer 110 and the annular seal 130. The first fluid conduit 115 preferably is an annular member fabricated from any number

of conventional commercially available materials such as, for example, oilfield country tubular goods, low alloy steel, carbon steel, or stainless steel. In a preferred embodiment, the first fluid conduit 115 includes one or more fluid inlets 125 for conveying fluidic materials from the annular fluid passage 120 into the chamber 175.

5 The annular fluid passage 120 is defined by and positioned between the interior surface of the first fluid conduit 115 and the exterior surface of the second fluid conduit 135. The annular fluid passage 120 is preferably adapted to convey fluidic materials such as cement, water, epoxy, lubricants, and slag mix at operating pressures and flow rates ranging from about 0 to 3,000 gallons/minute and 0 to 9,000 psi in order to optimally  
10 provide flow rates and operational pressures for the radial expansion process.

The fluid inlets 125 are positioned in an end portion of the first fluid conduit 115. The fluid inlets 125 preferably are adapted to convey fluidic materials such as cement, water, epoxy, lubricants, and slag mix at operating pressures and flow rates ranging from about 0 to 9,000 psi and 0 to 3,000 gallons/minute in order to optimally provide flow rates  
15 and operational pressures for the radial expansion process.

The annular seal 130 is coupled to the first fluid conduit 115 and the second fluid conduit 135. The annular seal 130 preferably provides a fluid seal between the interior surface of the first fluid conduit 115 and the exterior surface of the second fluid conduit 135. The annular seal 130 preferably provides a fluid seal between the interior surface of  
20 the first fluid conduit 115 and the exterior surface of the second fluid conduit 135 during relative axial motion of the first fluid conduit 115 and the second fluid conduit 135. The annular seal 130 may be any number of conventional commercially available seals such as, for example, O-rings, polypak seals (RTM), or metal spring energized seals. In a preferred embodiment, the annular seal 130 is a polypak seal available from Parker Seals.

25 The second fluid conduit 135 is coupled to the annular seal 130 and the mandrel 145. The second fluid conduit preferably is a tubular member fabricated from any number of conventional commercially available materials such as, for example, coiled tubing, oilfield country tubular goods, low alloy steel, stainless steel, or low carbon steel. In a preferred embodiment, the second fluid conduit 135 is adapted to convey fluidic materials  
30 such as cement, water, epoxy, lubricants, and slag mix at operating pressures and flow

rates ranging from about 0 to 9,000 psi and 0 to 3,000 gallons/minute in order to optimally provide flow rates and operational pressures for the radial expansion process.

The fluid passage 140 is coupled to the second fluid conduit 135 and the mandrel 145. In a preferred embodiment, the fluid passage 140 is adapted to convey fluidic 5 materials such as cement, water, epoxy, lubricants, and slag mix at operating pressures and flow rates ranging from about 0 to 9,000 psi and 0 to 3,000 gallons/minute in order to optimally provide flow rates and operational pressures for the radial expansion process.

The mandrel 145 is coupled to the second fluid conduit 135 and the mandrel launcher 150. The mandrel 145 preferably is an annular member having a conic section 10 fabricated from any number of conventional commercially available materials such as, for example, machine tool steel, ceramics, tungsten carbide, titanium or other high strength alloys. In a preferred embodiment, the angle of the conic section of the mandrel 145 ranges from about 0 to 30 degrees in order to optimally expand the mandrel launcher 150 and tubular member 155 in the radial direction. In a preferred embodiment, the surface of 15 the conic section ranges from about 58 to 62 Rockwell C in order to optimally provide high yield strength. In a preferred embodiment, the mandrel 145 is heat treated in order to optimally provide a hard outer surface and a resilient interior body in order to optimally provide abrasion resistance and fracture toughness. In an alternative embodiment, the mandrel 145 is expandible in order to further optimally augment the radial expansion 20 process.

The mandrel launcher 150 is coupled to the support member 105, the mandrel 145, and the tubular member 155. The mandrel launcher 150 preferably is a tubular member having a variable cross-section and a reduced wall thickness in order to facilitate the radial expansion process. In a preferred embodiment, the cross-sectional area of the 25 mandrel launcher 150 at one end is adapted to mate with the mandrel 145, and at the other end, the cross-sectional area of the mandrel launcher 150 is adapted to match the cross-sectional area of the tubular member 155. In a preferred embodiment, the wall thickness of the mandrel launcher 150 ranges from about 50 to 100 % of the wall thickness of the tubular member 155 in order to facilitate the initiation of the radial expansion process.

30 The mandrel launcher 150 may be fabricated from any number of conventional commercially available materials such as, for example, oilfield country tubular goods, low

allow steel, stainless steel, or carbon steel. In a preferred embodiment, the mandrel launcher 150 is fabricated from oilfield country tubular goods having higher strength but lower wall thickness than the tubular member 155 in order to optimally match the burst strength of the tubular member 155. In a preferred embodiment, the mandrel launcher 5 150 is removably coupled to the tubular member 155. In this manner, the mandrel launcher 150 may be removed from the wellbore 180 upon the completion of an extrusion operation.

In an alternative embodiment, the support member 105 and the mandrel launcher 150 are integrally formed. In this alternative embodiment, the support member 105 10 preferably terminates above the top of the packer 110. In this alternative embodiment, the fluid conduits 115 and/or 135 provide structural support for the apparatus 100, using the packer 110 to couple together the elements of the apparatus 100. In another embodiment, during the radial expansion process, the packer 110 may be unset and reset, after the slips 160 have anchored the tubular member 155 to the previous casing 170, within the tubular 15 member 155, between radial expansion operations. In this manner, the packer 110 is moved downhole and the apparatus 100 is re-stroked.

The tubular member 155 is coupled to the mandrel launcher, the slips 160 and the seals 165. The tubular member 155 preferably is a tubular member fabricated from any 20 number of conventional commercially available materials such as, for example, low alloy steel, carbon steel, stainless steel, or oilfield country tubular goods. In a preferred embodiment, the tubular member 155 is fabricated from oilfield country tubular goods.

The slips 160 are coupled to the outside surface of the tubular member 155. The slips 160 preferably are adapted to couple to the interior walls of a casing, pipeline or other structure upon the radial expansion of the tubular member 155. In this manner, the 25 slips 160 provide structural support for the expanded tubular member 155. The slips 160 may be any number of conventional commercially available slips such as, for example, RTTS packer tungsten carbide slips, RTTS packer wicker type mechanical slips or Model 3L retrievable bridge plug tungsten carbide upper mechanical slips. In a preferred embodiment, the slips 160 are RTTS packer tungsten carbide mechanical slips available 30 from Halliburton Energy Services. In a preferred embodiment, the slips 160 are adapted to support axial forces ranging from about 0 to 750,000 lbf.

The seals 165 are coupled to the outside surface of the tubular member 155. The seals 165 preferably provide a fluidic seal between the outside surface of the expanded tubular member 155 and the interior walls of a casing, pipeline or other structure upon the radial expansion of the tubular member 155. In this manner, the seals 165 provide a

5 fluidic seal for the expanded tubular member 155. The seals 165 may be any number of conventional commercially available seals such as, for example, nitrile rubber, lead, Aflas rubber, Teflon (RTM), epoxy, or other elastomers. In a preferred embodiment, the seals 165 are rubber seals available from numerous commercial vendors in order to optimally provide pressure sealing and load bearing capacity.

10 During operation of the apparatus 100, the apparatus 100 is preferably lowered into a wellbore 180 having a preexisting section of wellbore casing 170. In a preferred embodiment, the apparatus 100 is positioned with at least a portion of the tubular member 155 overlapping with a portion of the wellbore casing 170. In this manner, the radial expansion of the tubular member 155 will preferably cause the outside surface of the

15 expanded tubular member 155 to couple with the inside surface of the wellbore casing 170. In a preferred embodiment, the radial expansion of the tubular member 155 will also cause the slips 160 and seals 165 to engage with the interior surface of the wellbore casing 170. In this manner, the expanded tubular member 155 is provided with enhanced structural support by the slips 160 and an enhanced fluid seal by the seals 165.

20 As illustrated in FIG. 1b, after placement of the apparatus 100 in an overlapping relationship with the wellbore casing 170, a fluidic material 185 is preferably pumped into the chamber 175 using the fluid passage 120 and the inlet passages 125. In a preferred embodiment, the fluidic material is pumped into the chamber 175 at operating pressures and flow rates ranging from about 0 to 9,000 psi and 0 to 3,000 gallons/minute in order to

25 optimally provide flow rates and operational pressures for the radial expansion process. The pumped fluidic material 185 increases the operating pressure within the chamber 175. The increased operating pressure in the chamber 175 then causes the mandrel 145 to extrude the mandrel launcher 150 and tubular member 155 off of the face of the mandrel 145. The extrusion of the mandrel launcher 150 and tubular member 155 off of the face

30 of the mandrel 145 causes the mandrel launcher 150 and tubular member 155 to expand in

the radial direction. Continued pumping of the fluidic material 185 preferably causes the entire length of the tubular member 155 to expand in the radial direction.

In a preferred embodiment, the pumping rate and pressure of the fluidic material 185 is reduced during the latter stages of the extrusion process in order to minimize shock 5 to the apparatus 100. In a preferred embodiment, the apparatus 100 includes shock absorbers for absorbing the shock caused by the completion of the extrusion process.

In a preferred embodiment, the extrusion process causes the mandrel 145 to move in an axial direction 186. During the axial movement of the mandrel, in a preferred embodiment, the fluid passage 140 conveys fluidic material 190 displaced by the moving 10 mandrel 145 out of the wellbore 180. In this manner, the operational efficiency and speed of the extrusion process is enhanced.

In a preferred embodiment, the extrusion process includes the injection of a hardenable fluidic material into the annular region between the tubular member 155 and the bore hole 180. In this manner, a hardened sealing layer is provided between the 15 expanded tubular member 155 and the interior walls of the wellbore 180.

As illustrated in FIG. 1c, in a preferred embodiment, upon the completion of the extrusion process, the support member 105, packer 110, first fluid conduit 115, annular seal 130, second fluid conduit 135, mandrel 145, and mandrel launcher 150 are moved from the wellbore 180.

20 In an alternative embodiment, the apparatus 100 is used to repair a preexisting wellbore casing or pipeline. In this alternative embodiment, both ends of the tubular member 155 preferably include slips 160 and seals 165.

In an alternative embodiment, the apparatus 100 is used to form a tubular structural support for a building or offshore structure.

25 Referring now to FIGS. 2a, 2b, 2c, 2d, and 2e, an apparatus 200 for expanding a tubular member will be described. In a preferred embodiment, the apparatus 200 includes a support member 205, a mandrel launcher 210, a mandrel 215, a first fluid passage 220, a tubular member 225, slips 230, seals 235, a shoe 240, and a second fluid passage 245. In a preferred embodiment, the apparatus 200 is used to radially expand the mandrel 30 launcher 210 and tubular member 225. In this manner, the apparatus 200 may be used to form a wellbore casing, line a wellbore casing, form a pipeline, line a pipeline, form a

structural support member, or repair a wellbore casing, pipeline or structural support member. In a preferred embodiment, the apparatus 200 is used to clad at least a portion of the tubular member 225 onto a preexisting structural member.

The support member 205 is preferably coupled to the mandrel launcher 210. The 5 support member 205 preferably is a tubular member fabricated from any number of conventional commercially available materials such as, for example, oilfield country tubular goods, low alloy steel, carbon steel, or stainless steel. The support member 205, the mandrel launcher 210, the tubular member 225, and the shoe 240 are preferably selected to fit through a preexisting section of wellbore casing 275. In this manner, the 10 apparatus 200 may be positioned within the wellbore casing 275. In a preferred embodiment, the support member 205 is releasably coupled to the mandrel launcher 210. In this manner, the support member 205 may be decoupled from the mandrel launcher 210 upon the completion of an extrusion operation.

The mandrel launcher 210 is coupled to the support member 205 and the tubular member 225. The mandrel launcher 210 preferably is a tubular member having a variable 15 cross-section and a reduced wall thickness in order to facilitate the radial expansion process. In a preferred embodiment, the cross-sectional area of the mandrel launcher 210 at one end is adapted to mate with the mandrel 215, and at the other end, the cross-sectional area of the mandrel launcher 210 is adapted to match the cross-sectional area of 20 the tubular member 225. In a preferred embodiment, the wall thickness of the mandrel launcher 210 ranges from about 50 to 100 % of the wall thickness of the tubular member 225 in order to facilitate the initiation of the radial expansion process.

The mandrel launcher 210 may be fabricated from any number of conventional 25 commercially available materials such as, for example, oilfield country tubular goods, low allow steel, stainless steel, or carbon steel. In a preferred embodiment, the mandrel launcher 210 is fabricated from oilfield country tubular goods having higher strength but lower wall thickness than the tubular member 225 in order to optimally match the burst strength of the tubular member 225. In a preferred embodiment, the mandrel launcher 210 is removably coupled to the tubular member 225. In this manner, the mandrel 30 launcher 210 may be removed from the wellbore 260 upon the completion of an extrusion operation.

The mandrel 215 is coupled to the mandrel launcher 210. The mandrel 215 preferably is an annular member having a conic section fabricated from any number of conventional commercially available materials such as, for example, machine tool steel, ceramics, tungsten carbide, titanium or other high strength alloys. In a preferred 5 embodiment, the angle of the conic section of the mandrel 215 ranges from about 0 to 30 degrees in order to optimally expand the mandrel launcher 210 and the tubular member 225 in the radial direction. In a preferred embodiment, the surface of the conic section ranges from about 58 to 62 Rockwell C in order to optimally provide high yield strength. In a preferred embodiment, the mandrel 215 is heat treated in order to optimally provide a 10 hard outer surface and a resilient interior body in order to optimally provide abrasion resistance and fracture toughness. In an alternative embodiment, the mandrel 215 is expandible in order to further optimally augment the radial expansion process.

The fluid passage 220 is positioned within the mandrel 215. The fluid passage 220 is preferably adapted to convey fluidic materials such as cement, water, epoxy, 15 lubricants, and slag mix at operating pressures and flow rates ranging from about 0 to 9,000 psi and 0 to 3,000 gallons/minute in order to optimally provide flow rates and operational pressures for the radial expansion process. The fluid passage 220 preferably includes an inlet 265 adapted to receive a plug, or other similar device. In this manner, the interior chamber 270 above the mandrel 215 may be fluidically isolated from the 20 interior chamber 272 below the mandrel 215.

The tubular member 225 is coupled to the mandrel launcher 210, the slips 230 and the seals 235. The tubular member 225 preferably is a tubular member fabricated from any number of conventional commercially available materials such as, for example, low alloy steel, carbon steel, stainless steel, or oilfield country tubular goods. In a preferred 25 embodiment, the tubular member 225 is fabricated from oilfield country tubular goods.

The slips 230 are coupled to the outside surface of the tubular member 225. The slips 230 preferably are adapted to couple to the interior walls of a casing, pipeline or other structure upon the radial expansion of the tubular member 225. In this manner, the slips 230 provide structural support for the expanded tubular member 225. The slips 230 30 may be any number of conventional commercially available slips such as, for example, RTTS packer tungsten carbide mechanical slips, RTTS packer wicker type mechanical

slips, or Model 3L retrievable bridge plug tungsten carbide upper mechanical slips. In a preferred embodiment, the slips 230 are adapted to support axial forces ranging from about 0 to 750,000 lbf.

The seals 235 are coupled to the outside surface of the tubular member 225. The 5 seals 235 preferably provide a fluidic seal between the outside surface of the expanded tubular member 225 and the interior walls of a casing, pipeline or other structure upon the radial expansion of the tubular member 225. In this manner, the seals 235 provide a fluidic seal for the expanded tubular member 225. The seals 235 may be any number of conventional commercially available seals such as, for example, nitrile rubber, lead, Aflas 10 rubber, Teflon, epoxy or other elastomers. In a preferred embodiment, the seals 235 are conventional rubber seals available from various commercial vendors in order to optimally provide pressure sealing and load bearing capacity.

The shoe 240 is coupled to the tubular member 225. The shoe 240 preferably is a substantially tubular member having a fluid passage 245 for conveying fluidic materials 15 from the chamber 272 to the annular region 274 outside of the apparatus 200. The shoe 240 may be any number of conventional commercially available shoes such as, for example, a Super Seal II (RTM) float shoe, a Super Seal II Down-Jet float shoe, or a guide shoe with a sealing sleeve for a latch down plug modified in accordance with the teachings of the present disclosure. In a preferred embodiment, the shoe 240 is an 20 aluminum down-jet guide shoe with a sealing sleeve for a latch down plug, available from Halliburton Energy Services, modified in accordance with the teachings of the present disclosure, in order to optimally guide the tubular member 225 in the wellbore, optimally provide a fluidic seal between the interior and exterior diameters of the overlapping joint between the tubular members, and optimally facilitate the complete drilling out of the 25 shoe and plug upon the completion of the cementing and radial expansion operations.

During operation of the apparatus 200, the apparatus 200 is preferably lowered into a wellbore 260 having a preexisting section of wellbore casing 275. In a preferred embodiment, the apparatus 200 is positioned with at least a portion of the tubular member 225 overlapping with a portion of the wellbore casing 275. In this manner, the radial 30 expansion of the tubular member 225 will preferably cause the outside surface of the expanded tubular member 225 to couple with the inside surface of the wellbore casing

275. In a preferred embodiment, the radial expansion of the tubular member 225 will also cause the slips 230 and seals 235 to engage with the interior surface of the wellbore casing 275. In this manner, the expanded tubular member 225 is provided with enhanced structural support by the slips 230 and an enhanced fluid seal by the seals 235.

5        As illustrated in FIG. 2b, after placement of the apparatus 200 in an overlapping relationship with the wellbore casing 275, a fluidic material 280 is preferably pumped into the chamber 270. The fluidic material 280 then passes through the fluid passage 220 into the chamber 272. The fluidic material 280 then passes out of the chamber 272, through the fluid passage 245, and into the region 274. In a preferred embodiment, the fluidic material 280 is pumped into the chamber 270 at operating pressures and flow rates ranging from about 0 to 9,000 psi and 0 to 3,000 gallons/minute in order to optimally provide flow rates and operational pressures for the radial expansion process. In a preferred embodiment, the fluidic material 280 is a hardenable fluidic sealing material in order to form a hardened outer annular member around the expanded tubular member 225.

10      As illustrated in FIG. 2c, at some later point in the process, a ball 285, plug or other similar device, is introduced into the pumped fluidic material 280. In a preferred embodiment, the ball 285 mates with and seals off the inlet 265 of the fluid passage 220. In this manner, the chamber 270 is fluidically isolated from the chamber 272.

15      As illustrated in FIG. 2d, after placement of the ball 285 in the inlet 265 of the fluid passage 220, a fluidic material 290 is pumped into the chamber 270. The fluidic material is preferably pumped into the chamber 270 at operating pressures and flow rates ranging from about 0 to 9,000 psi and 0 to 3,000 gallons/minute in order to provide optimal operating efficiency. The fluidic material 290 may be any number of conventional commercially available materials such as, for example, water, drilling mud, cement, epoxy, or slag mix. In a preferred embodiment, the fluidic material 290 is a non-hardenable fluidic material in order to maximize operational efficiency.

20      Continued pumping of the fluidic material 290 increases the operating pressure within the chamber 270. The increased operating pressure in the chamber 270 then causes the mandrel 215 to extrude the mandrel launcher 210 and tubular member 225 off of the 25 conical face of the mandrel 215. The extrusion of the mandrel launcher 210 and tubular member 225 off of the conical face of the mandrel 215 causes the mandrel launcher 210

and tubular member 225 to expand in the radial direction. Continued pumping of the fluidic material 290 preferably causes the entire length of the tubular member 225 to expand in the radial direction.

In a preferred embodiment, the pumping rate and pressure of the fluidic material 290 is reduced during the latter stages of the extrusion process in order to minimize shock to the apparatus 200. In a preferred embodiment, the apparatus 200 includes shock absorbers for absorbing the shock caused by the completion of the extrusion process. In a preferred embodiment, the extrusion process causes the mandrel 215 to move in an axial direction 295.

As illustrated in FIG. 2e, in a preferred embodiment, upon the completion of the extrusion process, the support member 205, packer 210, first fluid conduit 215, annular seal 230, second fluid conduit 235, mandrel 245, and mandrel launcher 250 are removed from the wellbore 260. In a preferred embodiment, the resulting new section of wellbore casing includes the preexisting wellbore casing 275, the expanded tubular member 225, the slips 230, the seals 235, the shoe 240, and an outer annular layer 300 of hardened fluidic material.

In an alternative embodiment, the apparatus 200 is used to repair a preexisting wellbore casing or pipeline. In this alternative embodiment, both ends of the tubular member 255 preferably include slips 260 and seals 265.

In an alternative embodiment, the apparatus 200 is used to form a tubular structural support for a building or offshore structure.

In a preferred embodiment, the tubular members 155 and 225; shoes 240; mandrel launchers 150 and 210; and mandrels 145 and 215 are provided substantially as described in one or more of the following U.S. patents and applications: (1) utility patent 6,328,113, 25 having application number 09/440,338, attorney docket number 25791.9.02, filed on 11-16-1999, which claimed the benefit of the filing date of provisional patent application number 60/108,558, attorney docket number 25791.9, filed on 11-16-1998; (2) utility patent 6,497,289, having application number 09/454,139, attorney docket number 25791.3.02, filed on 12-3-1999, which claimed the benefit of the filing date of provisional 30 patent application number 60/111,293, attorney docket number 25791.3, filed on 12-7-1998; (3) utility patent application number 09/502,350, attorney docket number

25791.8.02, filed on 2-10-2000, which claimed the benefit of the filing date of provisional patent application number 60/119,611, attorney docket number 25791.8, filed on 2-11-1999; (4) provisional patent application number 60/121,702, attorney docket number 25791.7, filed on 2-25-1999; (5) provisional patent application number 60/121,841,

5 attorney docket number 25791.12, filed on 2-26-1999; (6) provisional patent application number 60/121,907, attorney docket number 25791.16, filed on 2-26-1999; (7) provisional patent application number 60/124,042, attorney docket number 25791.11, filed on 3-11-1999; (8) provisional patent application number 60/131,106, attorney docket number 25791.23, filed on 4-26-1999; (9) provisional patent application number

10 60/137,998, attorney docket number 25791.17, filed on 6-7-1999; (10) provisional patent application number 60/143,039, attorney docket number 25791.26, filed on 7-9-1999; (11) provisional patent application number 60/146,203, attorney docket number 25791.25, filed on 7-29-1999; (12) provisional patent application number 60/154,047, attorney docket number 25791.29, filed on 9-16-1999; (13) provisional patent application number

15 60/159,082, attorney docket number 25791.34, filed on 10-12-1999; (14) provisional patent application number 60/159,039, attorney docket number 25791.36, filed on 10-12-1999; (15) provisional patent application number 60/159,033, attorney docket number 25791.37, filed on 10-12-1999; (16) provisional patent application number 60/162,671, attorney docket number 25791.27, filed on 11-01-1999.

20 Although illustrative embodiments of the invention have been shown and described, a wide range of modification, changes and substitution is contemplated in the foregoing disclosure. In some instances, some features of the present invention may be employed without a corresponding use of the other features. Accordingly, it is appropriate that the appended claims be construed broadly and in a manner consistent

25 with the scope of the invention.

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20

**TABLE FOR CONVERSION TO METRIC UNITS**

- 0 to 750,000 lbf. (0 to 51,710.67 bar)
- 0 to 9,000 psi (0 to 620.528 bar)
- 5 0 to 3,000 gallons/minute (0 to 11356.24 litres/minute)

## Claims

1. A method of coupling a tubular member to a preexisting structure, comprising:  
positioning the tubular member in an overlapping relationship to the preexisting  
5 structure;  
placing a mandrel within the tubular member;  
pressurizing a region within the tubular member above the mandrel; and  
displacing the mandrel with respect to the tubular member.
- 10 2. The method of claim 1, further comprising:  
removing fluids within the tubular member that are displaced by the displacement  
of the mandrel.
- 15 3. The method of claim 2, wherein the removed fluids pass inside the region.
4. The method of claim 1, wherein the volume of the region increases.
5. The method of claim 1, further including sealing off the region.
- 20 6. The method of claim 5, wherein sealing off the region includes sealing a stationary  
member and sealing a non-stationary member.
7. The method of claim 1, further including conveying a first fluid in a first direction  
along an axis of the tubular member, and a second fluid in a second direction along the  
25 axis, the first direction being different than the second direction.
8. The method of claim 1, further including conveying a pressurized fluid in a first  
direction along an axis of the tubular member, and a non-pressurized fluid in a second  
direction along the axis, the first direction being different than the second direction.

9. The method of claim 1, wherein the pressurizing is provided at operating pressures ranging from 0 to 620.528 bar (0 to 9,000 psi).
10. The method of claim 1, wherein the pressurizing is provided at flow rates ranging from 0 to 11356.24 litres/minute (0 to 3,000 gallons/minute).
11. An apparatus for radially expanding a tubular member, comprising:
  - a first tubular member;
  - a second tubular member positioned within the first tubular member;
  - 10 a third tubular member movably coupled to and positioned within the second tubular member;
  - a first annular sealing member for sealing an interface between the first and second tubular members;
  - a second annular sealing member for sealing an interface between the second and 15 third tubular members; and
  - a mandrel positioned within the first tubular member and coupled to an end of the third tubular member.
12. The apparatus of claim 11, further including an annular chamber defined by the first 20 tubular member, the second tubular member, the third tubular member, the first annular sealing member, the second annular sealing member, and the mandrel.
13. The apparatus of claim 11, further including an annular passage defined by the second tubular member and the third tubular member.
- 25 14. The apparatus of claim 11, further including a fluid passage contained within the third tubular member and the mandrel.
15. The apparatus of claim 11, further including one or more sealing members coupled 30 to an exterior surface of the first tubular member.

16. The apparatus of claim 11, further including:

an annular chamber defined by the first tubular member, the second tubular member, the third tubular member, the first annular sealing member, the second annular sealing member, and the mandrel; and

5 an annular passage defined by the second tubular member and the third tubular member.

17. The apparatus of claim 16, wherein the annular chamber and the annular passage are fluidically coupled.

10

18. The apparatus of claim 11, further including one or more slips coupled to the exterior surface of the first tubular member.

19. The apparatus of claim 11, wherein the mandrel includes a conical surface.

15

20. The apparatus of claim 19, wherein the angle of attack of the conical surface ranges from 0 to 30 degrees.

21. The apparatus of claim 19, wherein the conical surface has a surface hardness 20 ranging from 58 to 62 Rockwell C.

22. An apparatus, comprising:

a first tubular member; and

a second tubular member coupled to the first tubular member

25 wherein the second tubular member is positioned in an overlapping relationship to the first tubular member;

a mandrel within the second tubular member;

a pressurized region within the second tubular member above the mandrel; and

a mechanism adapted for displacing the mandrel with respect to the second tubular

30 member.

23. The apparatus of claim 22, further comprising:  
a mechanism for removing fluids within the second tubular member that are  
displaced by the displacement of the mandrel.

5 24. The apparatus of claim 23, wherein the removed fluids pass inside the pressurized  
region.

25. The apparatus of claim 22, wherein the volume of the pressurized region increases.

10 26. The apparatus of claim 22, further comprising a sealing mechanism adapted for  
sealing off the pressurized region.

27. The apparatus of claim 26, wherein sealing off the pressurized region includes  
sealing a stationary member and sealing a non-stationary member.

15 28. The apparatus of claim 22, further comprising a mechanism for conveying a first  
fluid in a first direction along an axis of the second tubular member, and a second fluid in  
a second direction along the axis, the first direction being different than the second  
direction.

20 29. The apparatus of claim 22, further comprising a mechanism for conveying a  
pressurized fluid in a first direction along an axis of the second tubular member, and a  
non-pressurized fluid in a second direction along the axis, the first direction being  
different than the second direction.

25 30. The apparatus of claim 22, wherein the pressurizing is provided at operating  
pressures ranging from 0 to 620.528 bar (0 to 9,000 psi).

30 31. The apparatus of claim 22, wherein the pressuring is provided at flow rates ranging  
from 0 to 11356.24 litres/minute (0 to 3,000 gallons/minute).

32. A method of coupling a tubular member to a preexisting structure, comprising:  
preforming the tubular member to include a first portion, a second portion and a  
third portion;  
placing a mandrel within the second portion of the tubular member;  
5 positioning the tubular member in an overlapping relationship to the preexisting  
structure;  
pressurizing a region within the tubular member above the mandrel; and  
displacing the mandrel with respect to the tubular member;  
wherein the inside diarneter of the second portion of the tubular member is greater  
10 than the inside diameters of the first and third portions of the tubular member.

33. The method of claim 32, wherein the pressurizing is provided at operating pressures  
ranging from 0 to 620.528 bar (0 to 9,000 psi).

15 34. The method of claim 32, wherein the pressurizing is provided at flow rates ranging  
from 0 to 11356.24 litres/minute (0 to 3,000 gallons/minute).

35. The method of claim 32, wherein the tubular member is expanded beginning at an  
upper portion of the tubular member.  
20

36. An apparatus for radially expanding a tubular member, comprising:  
a first tubular member;  
a second tubular member coupled to the first tubular member;  
a third tubular member coupled to the second tubular member; and  
25 a mandrel positioned within the second tubular member and coupled to an end  
portion of the third tubular member;  
wherein the inside diameter of the second tubular member is greater than the inside  
diameters of the first and third tubular members.

30 37. The apparatus of claim 36, wherein the mandrel includes a fluid passage having an  
inlet adapted to receive a fluid stop member.

38. The apparatus of claim 36, further including one or more slips coupled to the exterior surface of the third tubular member.

5 39. The apparatus of claim 36, wherein the mandrel includes a conical surface.

40. The apparatus of claim 39, wherein the angle of attack of the conical surface ranges from 0 to 30 degrees.

10 41. The apparatus of claim 39, wherein the conical surface has a surface hardness ranging from 58 to 62 Rockwell C.

42. An apparatus, comprising:  
a preexisting structure; and

15 a tubular member coupled to the preexisting structure,  
the tubular member to include a first portion, a second portion and a third portion;  
a mandrel within the second portion of the tubular member;  
the tubular member in an overlapping relationship to the preexisting structure;  
a pressurized region within the tubular member above the mandrel; and

20 a mechanism for displacing the mandrel with respect to the tubular member;  
wherein the inside diameter of the second portion of the tubular member is greater than the inside diameters of the first and third portions of the tubular member.

43. The apparatus of claim 42, wherein the pressurizing is provided at operating pressures ranging from 0 to 620.528 bar (0 to 9,000 psi).

25

44. The method of claim 42, wherein the pressurizing is provided at flow rates ranging from 0 to 11356.24 litres/minute (0 to 3,000 gallons/minute).

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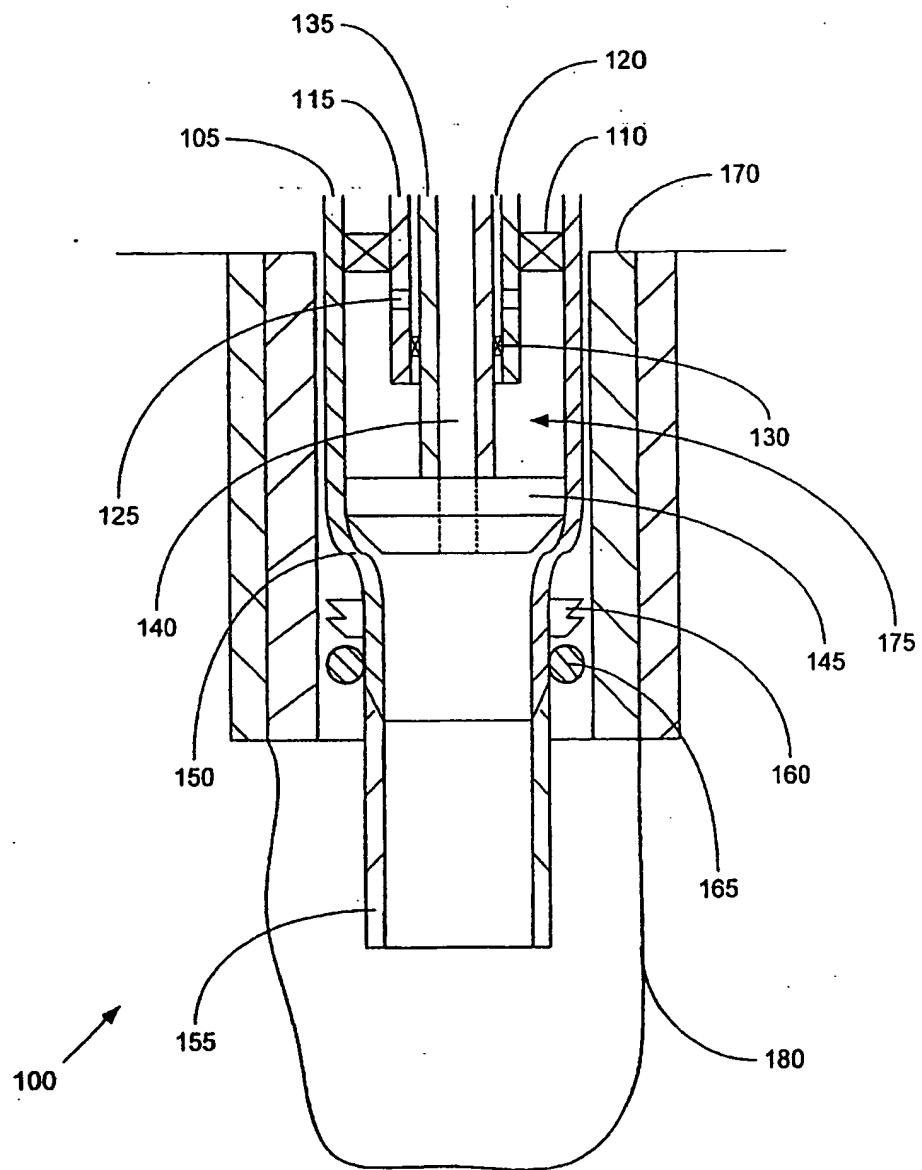


FIG. 1a

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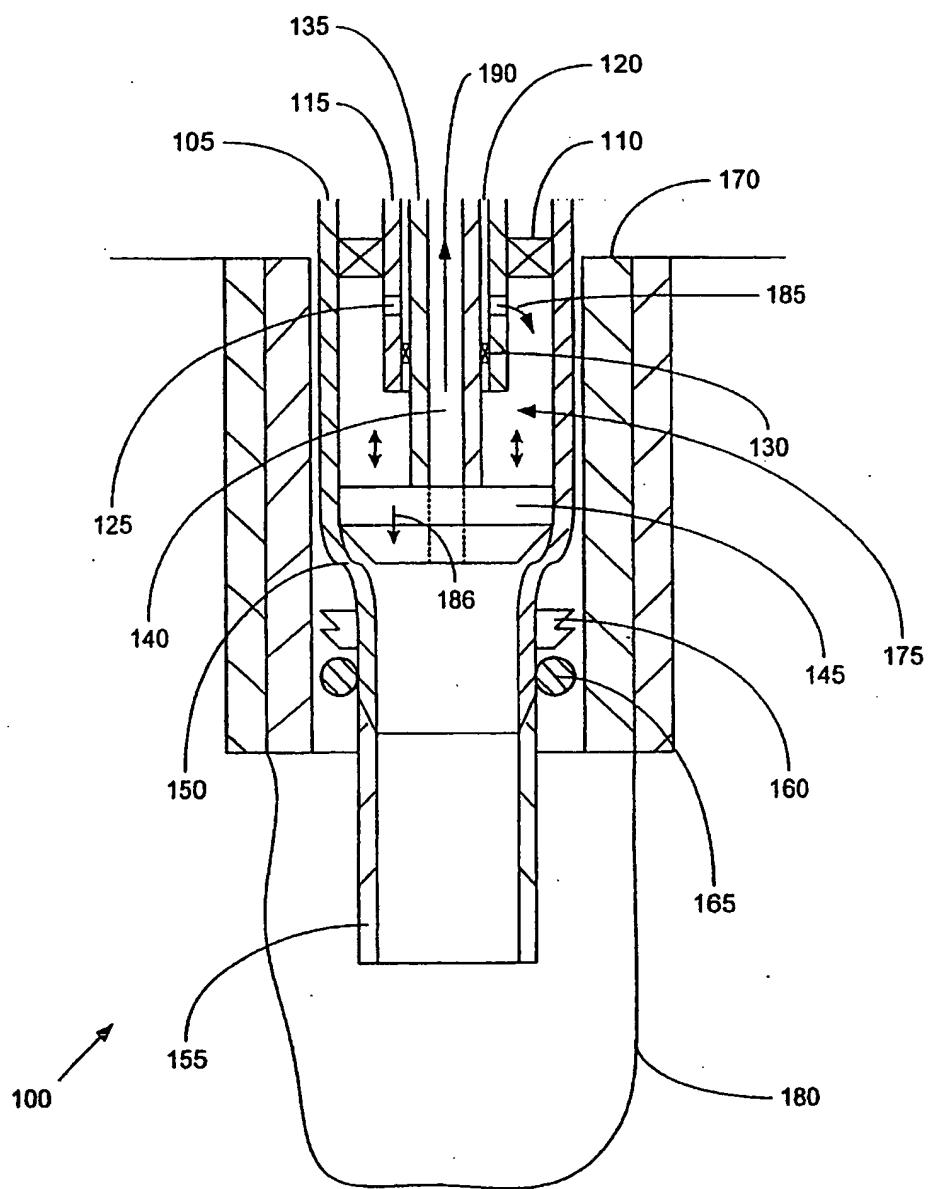


FIG. 1b

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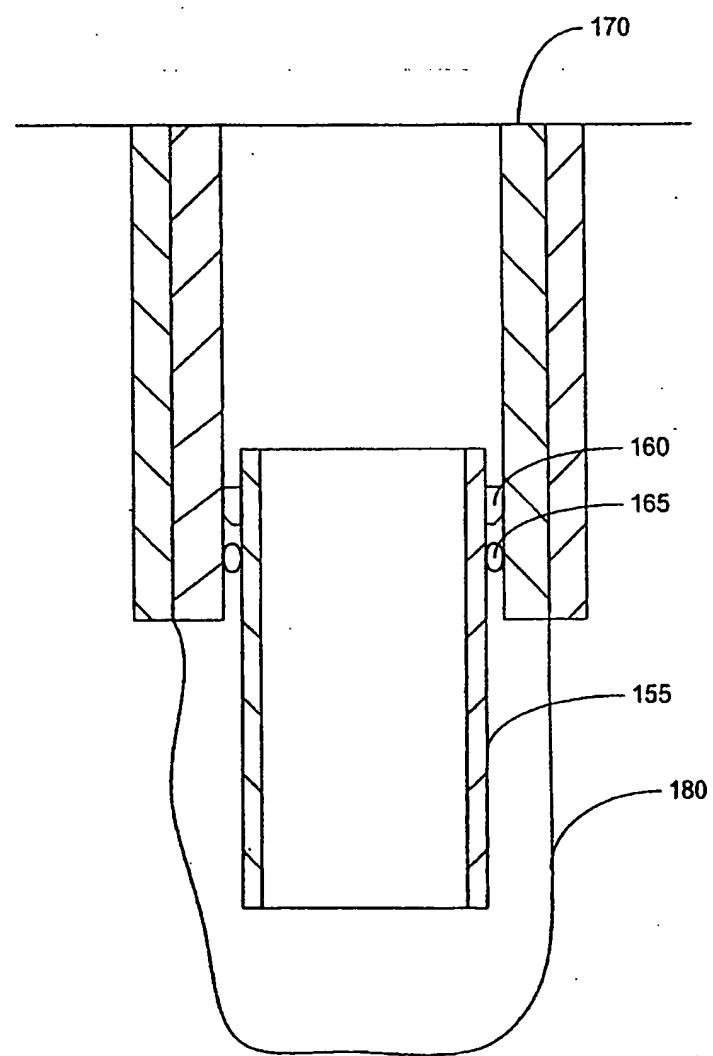
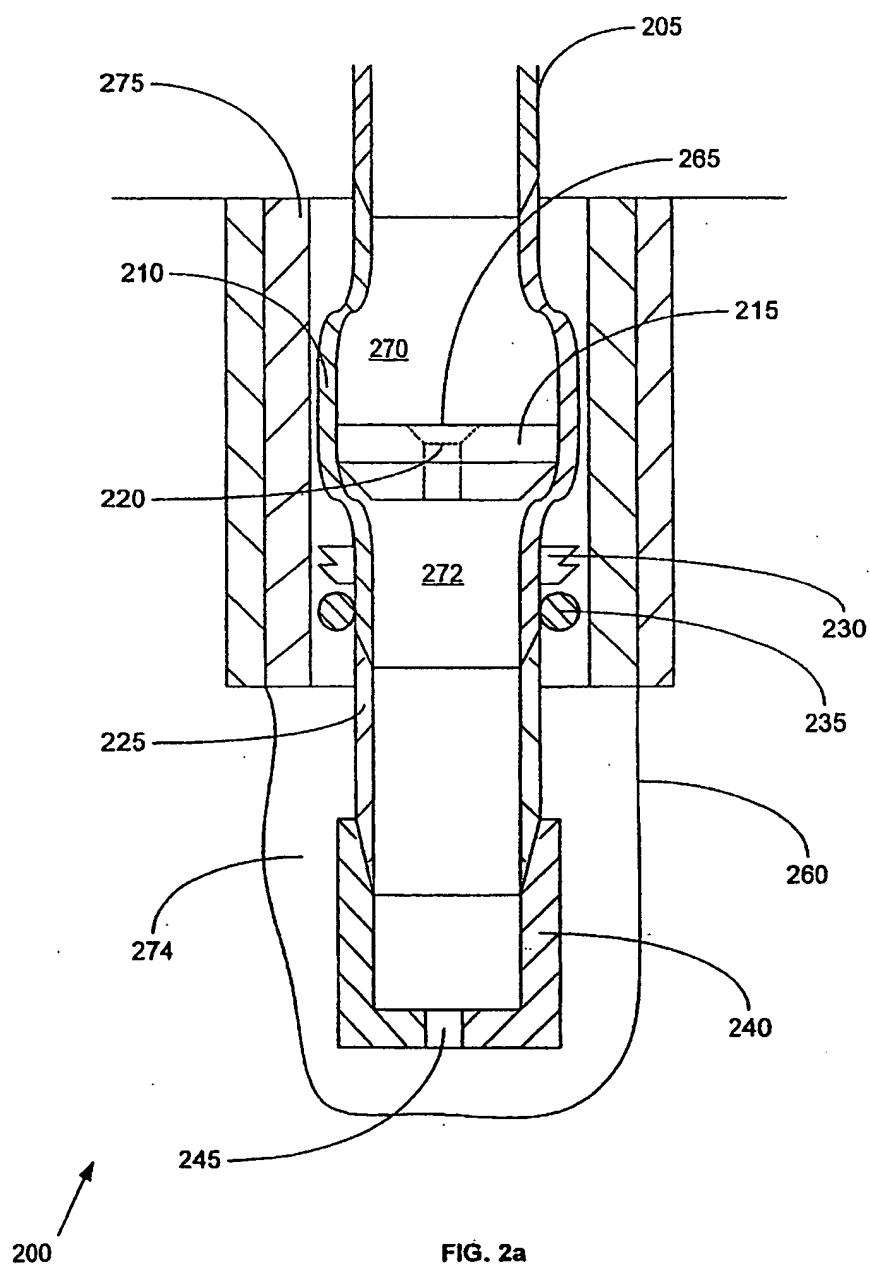


FIG. 1c

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16 +1.04

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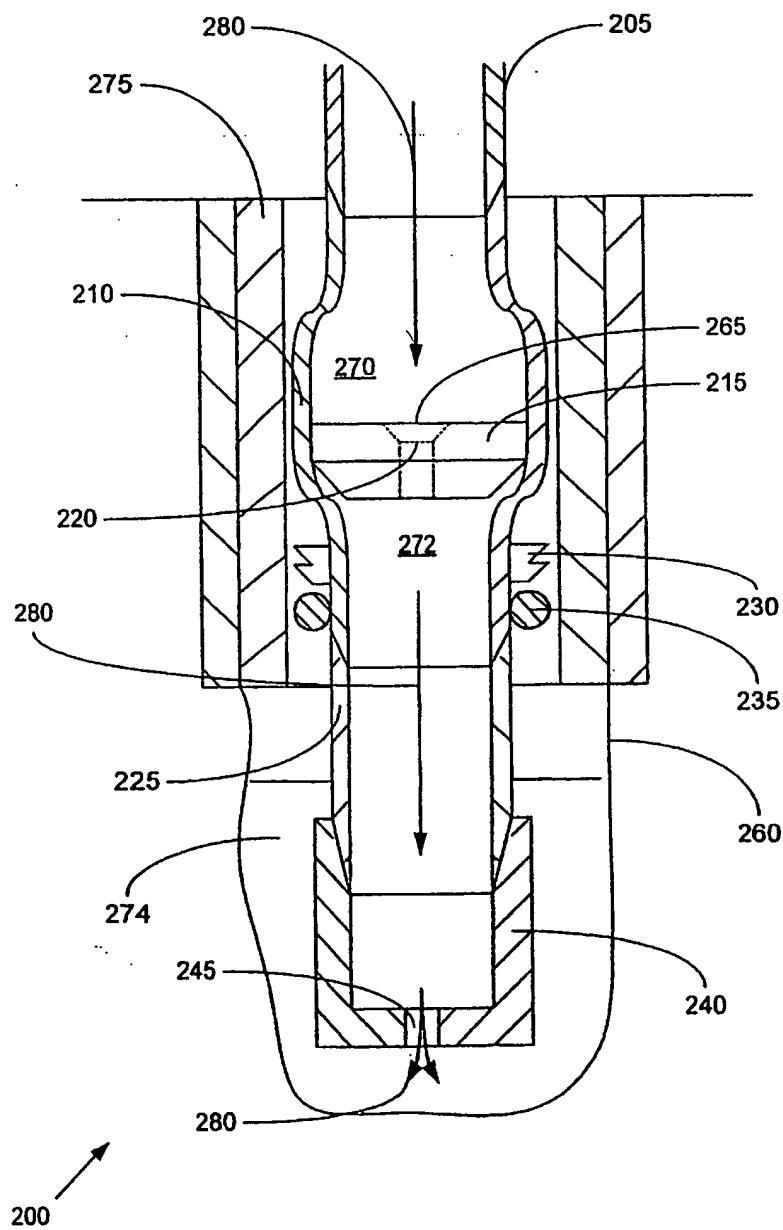
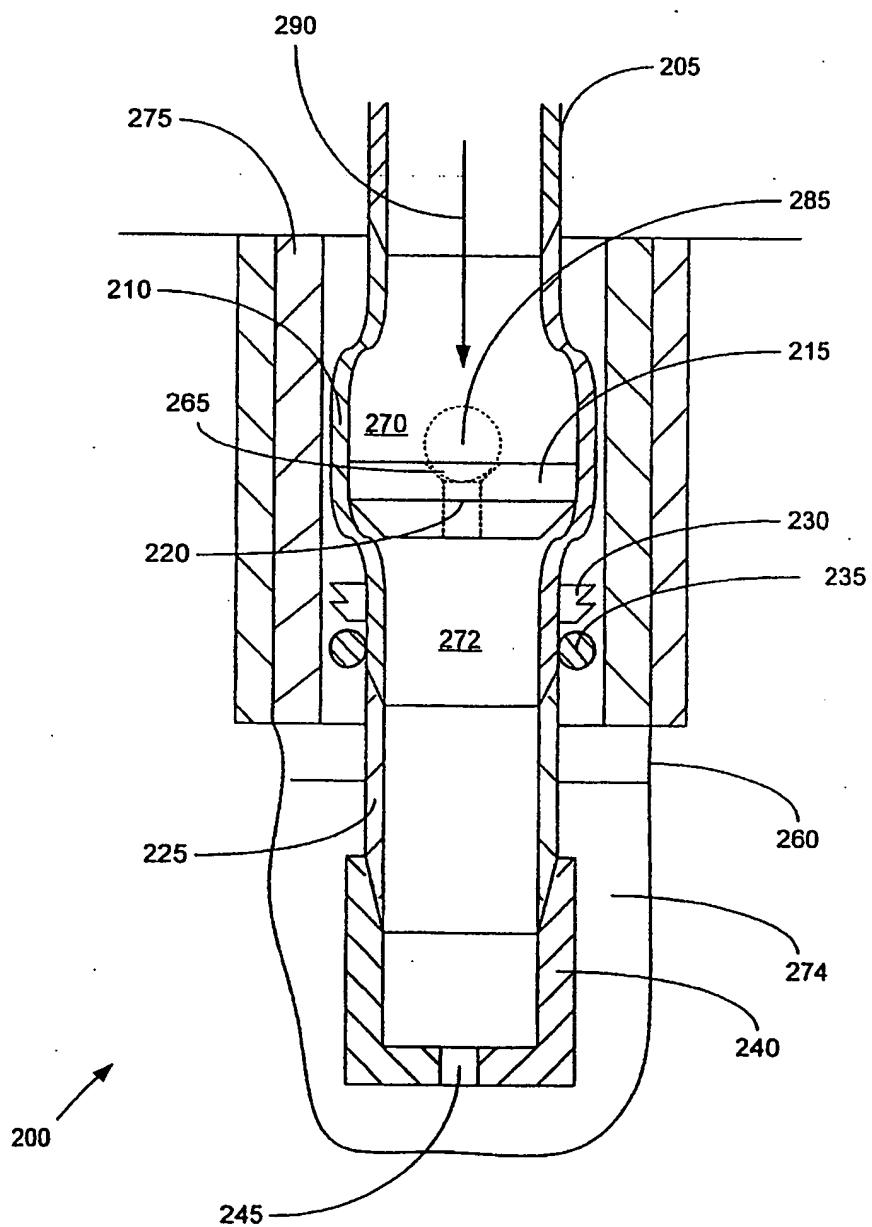


FIG. 2b

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**FIG. 2c**

16 ± 0.04

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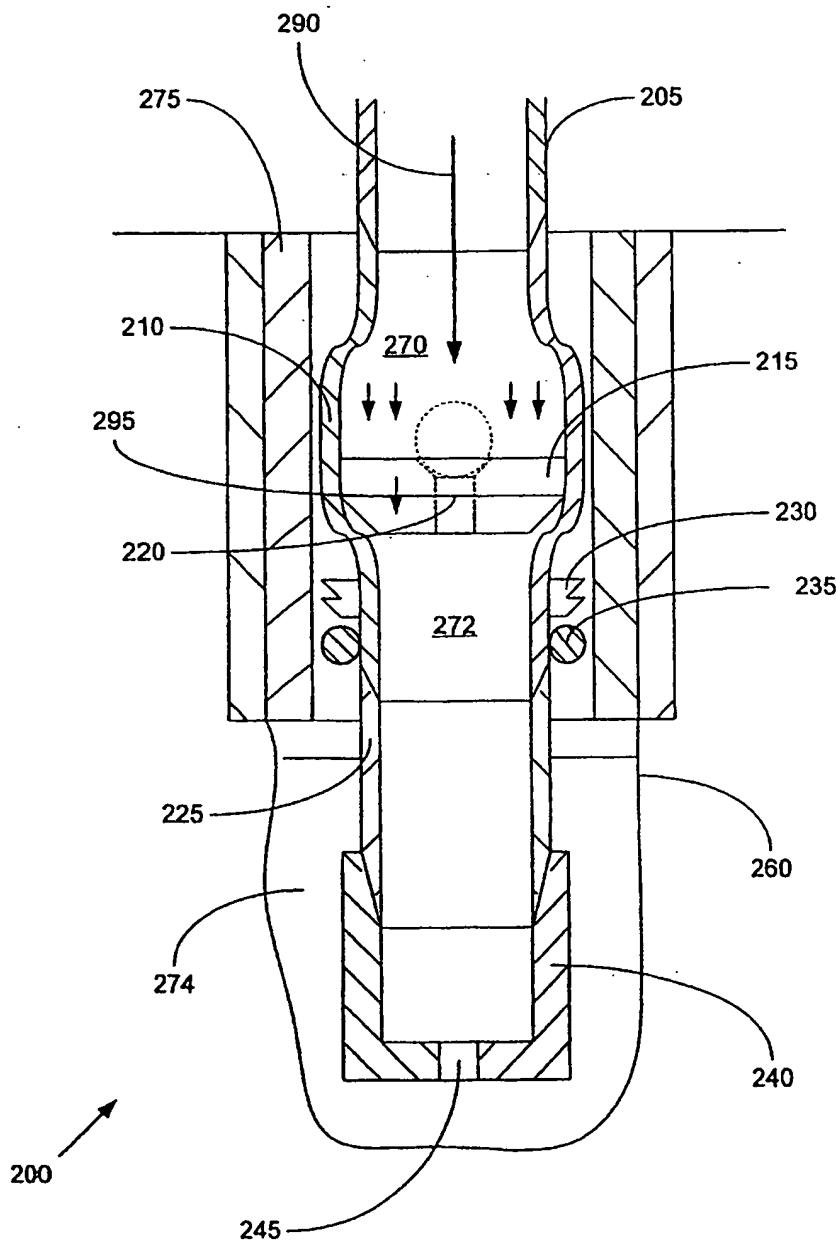


FIG. 2d

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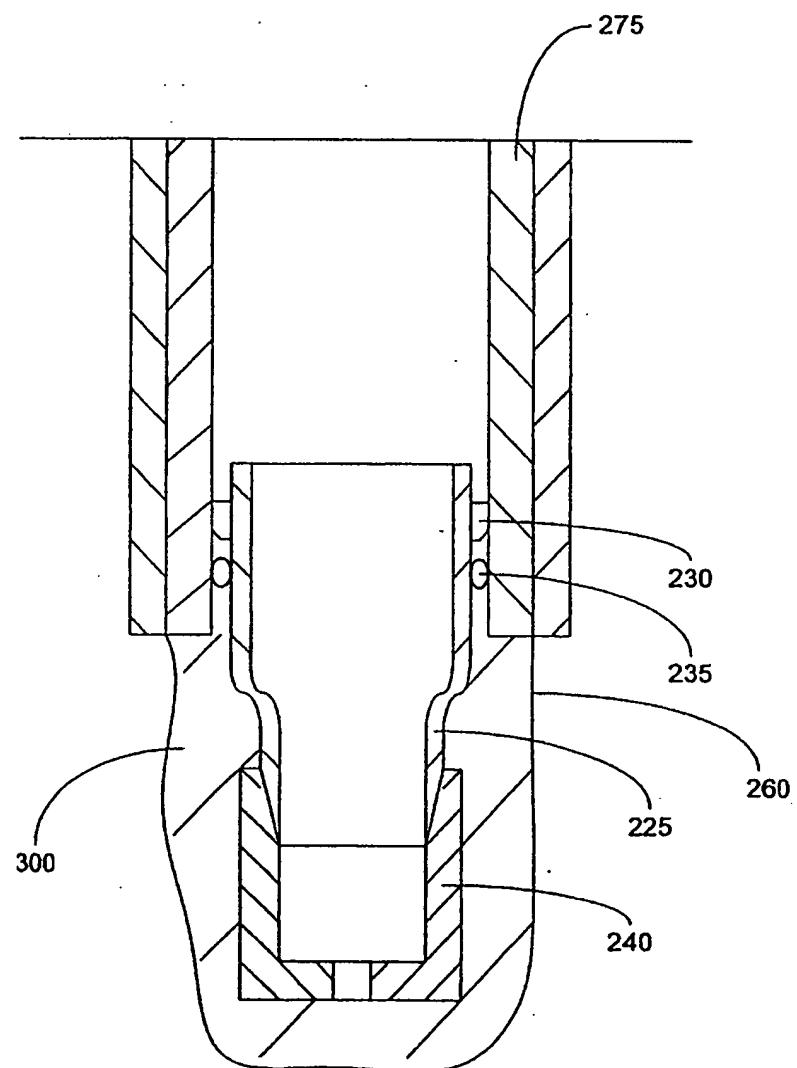


FIG. 2e

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